

ON THE AUTOROTATION OF ANIMAL WINGS

Victor Manuel Ortega-Jimenez^{1*}, Antonio Martín-Alcántara², Ramon Fernandez-Feria², Robert Dudley^{1,3}

¹ Department of Integrative Biology, University of California, Berkeley, Berkeley, CA 94720 USA

² Universidad de Málaga, Andalucía Tech, E. T. S. Ingeniería Industrial, Málaga, Spain

³ Smithsonian Tropical Research Institute, Balboa, Republic of Panama

*Corresponding author: ornithopterus@gmail.com

Abstract. Botanical samaras spin about their center of mass and create vertical aerodynamic forces which slow their rate of descent. Descending autorotation of animal wings, however, has never been documented. We report here that isolated wings from Anna's Hummingbirds, and also from ten species of insects, can stably autorotate and achieve descent speeds and aerodynamic performance comparable to those of samaras. A hummingbird wing loaded at their base with the equivalent of 50% of the bird's body mass descended only twice as fast as an unloaded wing, and rotated at frequencies similar to those of the wings in flapping flight. We found that even entire dead insects could stably autorotate depending on their wing postures. Feather removal trials showed no effect on descent velocity when the secondary feathers were removed from hummingbird wings. By contrast, partial removal of wing primaries substantially improved performance, except when only the outer primary was present. A scaling law for the aerodynamic performance of autorotating wings is well supported if the wing aspect ratio and the relative position of the spinning axis from the wing base are included. Autorotation is a useful and practical method that can be used to explore the aerodynamics of wing design.

Keywords: aerodynamics, feathers, insects, samaras, scaling

1. BACKGROUND

Many samaras descend at impressively low speeds while spinning around their center of gravity, and thereby maximizing dispersal distances from their source. Performance and stability in autorotation vary with shape, roughness, and camber of the lifting surface, and benefit from a mass distribution concentrated at the wing root and at the one-third chord length behind the leading edge of the wing [1, 2]. Early studies of samara descent aerodynamics [3] suggested unsteady mechanisms for lift production. A leading edge vortex (LEV), initially documented on small animal fliers [4–6], was then shown to underpin the high lift coefficients of autorotating seeds [7–9]. Moreover, comparison between autorotating and gliding samaras suggest that the former group can achieve longer flight times at higher weight loads [7, 10]. Animal flight research has long been used rotation as a theoretical proxy to characterize the aerodynamic performance of flapping wings (e.g. actuator disk theory; [11]), and the similarities in shape, aerodynamic performance, and unsteady lift mechanisms between plant seeds and animal wings have been variously noted [1–3, 7]. However, autorotation of animal wings has not yet been experimentally studied, even though this method, in comparison with modern experimental and computational approaches, is an elegant way for characterizing wing aerodynamics (e.g. the lift-to-drag ratio, LEV presence, and stability) and allows practical manipulative experiments which can be challenging to conduct on live animals. For example, wing autorotation can be used to explore the effects of ablation (as occurs during avian molting or with wing damage), as well as the forced rotations of isolated insect wings by adding weights (originally proposed by [3]). Autorotation performance also can be used to derive scaling relationships among different wings, as recently carried out for hovering insects [12]. Finally, performance comparison between winged seeds and animal wings may yield insight into low Re aerodynamics and into the convergent evolution of biological wing-like designs.

Here, we evaluate autorotation performance of isolated wings from ten insect species, and from

Anna's Hummingbirds (*Calypte anna*), to compare with published data on autorotating plant seeds. Furthermore, to understand the effects of ablation and mass loading on autorotation kinematics and aerodynamics, we carried out the following two experiments: different feathers from entire hummingbird wings were removed to understand their relative contributions to lift generation, and artificial weights were attached to the base of a hummingbird wing to match the wing loading of flying hummingbirds, so as to compare with the biomechanics of autorotation with flapping wings. We also tested if freshly killed insects with both wings intact could achieve stable autorotation. Finally, using a recent scaling law for the lift production of hovering insects [12], we derived general relationships for the autorotation of seeds and animal wings.

2. MATERIALS AND METHODS

A vertical wind tunnel was used, as in earlier studies of samaras [3], to explore wing autorotation. The cross-sectional area of the circular working section was approximately 490 cm² (i.e. ~12.5 cm radius), and a fine mesh was placed on the jet exit to minimize turbulence. Airspeed set in the wind tunnel when wings achieved stable autorotation was assumed to be the descent speed (U). Time per meter of descent (T_d) is then the inverse of the descent speed. We filmed stably autorotating wings at filming frequencies from 120–500 frames/s using a high-speed cameras (either X-PRI cameras (AOS Technologies, or HiSpec cameras (Fasttec Imaging)), and then analyzed wing kinematics (i.e., rotational frequency and coning angle) following standard methods [3].

Four wings from different male Anna's Hummingbirds were obtained from the frozen salvage collections of the Museum of Vertebrate Zoology, University of California, Berkeley. Hummingbird wings were cut using a scalpel at the shoulder, and were dried with the flight feathers in an approximately mid-stroke position. A small portion of the flight muscle was left attached to the wing,

and was then progressively trimmed until the wing effected stable autorotation within the wind tunnel jet. Similarly, adult insects were collected live in Berkeley, California, and forewings were cut progressively at their base from ten study taxa: Familiar Bluet (*Enallagma civile*), American Cockroach (*Periplaneta americana*), Bluebottle Fly (*Calliphora vomitoria*), Hawkmoth (*Manduca sexta*), Syrphus Hoverfly (*Syrphus opinator*), Umber Skipper (*Poanes melane*), Passion Butterfly (*Agraulis vanillae*), Monarch Butterfly (*Danaus plexippus*), Red Skimmer (*Libellula saturata*), and Marsh Crane-fly (*Tipula oleracea*). We took pictures of each sampled wing to determine morphometrics using the Matlab program wingImageProcessor 1.1 (<http://www.unc.edu/~thedrick/software3.html>; see Figure SA, Table 1). Wing mass (m_w) was measured using either a Sartorius CP2P microbalance (accuracy of 0.001 mg) for the smaller wings, or an Ohaus balance (accuracy of 0.01 g) for larger wings. Wing loading was then calculated as the ratio of wing weight ($W=m_w g$) to the wing area (S). Spanwise mass distribution for hummingbird wings was obtained from a published study [13], and was used to calculate the moment of inertia I from its spinning axis.

The effects of feather removal on autorotation were studied for three hummingbird wings, from each of which were removed first all the secondary feathers, then the primaries p1 to p5, and finally the primaries p6 to p9 (Figure SB). Each of these conditions with variable feather removal were studied for wing kinematics (i.e., three treatments), and were compared with the unmanipulated control. Effects of variable wing loading were studied by gluing small metal cylinders (0.9 cm in diameter; Figure SC) onto a metal wire (0.1 mm in diameter, length 0.5 cm, and with mass of 0.1 g) inserted into the proximal end of the humerus of the wing. Cylinder masses were either 1.1 g or 2.2 g, which values correspond approximately to one quarter and one half the mass of a male Anna's Hummingbird, respectively [13]. Moments of inertia for wings thus loaded were calculated including this extra weight at the wing base.

For statistical analyses, published data on descent speed and wing loading data for various samaras were first obtained from various references [1, 3, 7, 14–17]; values of the Strouhal number (see below) were taken from reference [3]. We then used an ANCOVA to test for difference in the slopes of regressions lines relating descent time versus wing loading for published samara data and the aggregated data from all animal wings studied here. To test for effects of feather removal on autorotation kinematics we used a repeated-measured ANOVA, followed by Tukey pairwise contrast when required. All statistical analysis were carried out in R v.3.0.2 [18].

3. RESULTS

Descriptive morphology and kinematic results for all tested animal wings are presented in Table 1. All tested wings could stably autorotate within the wind tunnel test area (see Video S1). In particular, we found that wings from the insect orders Odonata and Lepidoptera presented the lowest descent rates in comparison with other animal wings and most plant seeds. By contrast, the wings of smaller Diptera had the highest descent speeds. Both animal wings and botanical samaras exhibitedly shorter descent times at higher wing loadings W/S (Fig. 1; Supplementary Video S1), but animal wings overall presented a significant more shallow regression slope (i.e., -0.28 vs. -0.46), and thus tended to descend more slowly at high values of wing loading relative to loaded samaras (ANCOVA, $F_{1,287} = 14.2$, $P < 0.001$). Overall, removal of feathers from hummingbird wings significantly influenced descent speed ($F_{3,6}=24.9$, $P<0.001$), rotational frequency ($F_{3,6}=12.8$, $P<0.01$), coning angle ($F_{3,6}=31.6$, $P<0.001$), and tip velocity during rotation ($F_{3,6}=9.8$, $P=0.01$) (Figure 2). Removal of the secondaries influenced none of these kinematic variables (post-hoc test, $P>0.5$ for all variables), but removal of primaries P1 – P5 reduced the descent speed ($P<0.001$), increased the rotational frequency and tip velocity ($P<0.001$ in both cases), and left the coning angle unchanged ($P>0.05$). Wings with only the outer primary (p10)

present could nonetheless autorotate (Video S2), but with increases in all aforementioned variables ($P < 0.01$ for all contrasts). A hummingbird wing loaded with approximately 25% and 50% of a hummingbird's body mass increased descent speed by 65% and 100%, respectively, compared to the unloaded wing (Table 1, Video S3). We also observed that entire dead insects could stably autorotate depending on their fixed wing position. A freshly killed hawkmoth autorotated with a descent velocity of 3.1 m/s when its wings were positioned at either extreme of a wingbeat (i.e., at the end of a downstroke or upstroke), while a freshly killed hoverfly autorotated at a descent velocity of 2.3 m/s when both wings were positioned in a resting posture (Video S4).

4. DIMENSIONAL ANALYSIS AND SCALING LAWS

The aerodynamic performance of a rotating seed or wing can be characterized by a Strouhal number (i.e., the ratio of rotational to descent speeds, which is inversely proportional to the advance ratio), because this parameter determines rates of vortex shedding and thus propulsive efficiency. Here the Strouhal number is defined as:

$$St = \frac{nr}{U}, \quad (1)$$

where n is the rotational frequency and r the effective radius of gyration. St was between 0.2 and 0.4 for the majority of wings studied here (except for the hawkmoth with a value of 0.9; see Figure 3), as similarly been reported for forward flight in a variety of volant taxa at which maximal thrust efficiency occurs [19–24]. Experiments with oscillating airfoils indicate that maximal thrust efficiency occurs at $0.25 < St < 0.4$ [24], which is approximately the same range that has been observed in animal fliers during forward flight [23].

The steady descent velocity U of an autorotating wing or seed is expected to be a function of the

gyration frequency n , weight W , gyration radius r , wing surface S , fluid viscosity μ and density ρ , and other geometrical parameters such as the coning angle θ and the offset distance x_0 (see Figure 4); i.e.,

$$U=U(n,W,r,S,\mu,\rho,\theta,x_0). \quad (2)$$

r is here identified with the effective radius of gyration, so $r=(e - x_0)\cos(\theta)$, with e being the wing span (see Figure 4) which is not included in (2) because we instead use S and r .

Dimensional analysis provides the simplest functional relationship between these parameters. Since we are mostly interested here in the Strouhal number (eq. 1), we use n , r and ρ as the dimensional independent parameters. Applying the Buckingham Pi theorem [25],

$$\frac{U}{nr} = f\left(\frac{W}{\rho r^4 n^2}, \frac{S}{r^2}, \frac{\mu}{\rho r^2 n}, \theta, \frac{x_0}{r}\right) \quad (3)$$

However, in addition to the Strouhal number and θ , it is convenient to use the following related dimensionless parameters:

$$\overline{W} = \frac{W}{S} \frac{1}{\rho U_t^2} = \frac{W}{S} \frac{1}{\rho (2\pi nr)^2}, \quad (4)$$

$$\Lambda = \frac{e}{c}, \quad (5)$$

$$\text{Re} = \frac{\rho U_t r}{\mu} = \frac{2\pi\rho r^2 n}{\mu}, \quad (6)$$

$$\phi = \frac{e^{-x_0}}{e}, \quad (7)$$

so that (3) can be conveniently written as:

$$\text{St} = \text{St}(\overline{W}, \Lambda, \text{Re}, \theta, \phi). \quad (8)$$

In this relationship, \overline{W} is a non-dimensional wing loading scaled with the tangential (i.e., horizontal) wingtip velocity $U_t = 2\pi nr$, Λ is the aspect ratio of the wing, \bar{c} the mean chord, with $S = e\bar{c}$, Re is the Reynolds number based on U_t , and ϕ is the dimensionless offset of the wing base from the rotational axis (see Figure 4). Table 2 summarizes the values of these non-dimensional parameters in all the reported cases. Typically, $\text{Re} \gg 1$ for all the wings considered here, so that Re is not a characteristic parameter and one may neglect its effect on St (see [26]). Therefore eq. (8) may be written as:

$$\text{St} \sim \text{St}(\overline{W}, \Lambda, \theta, \phi). \quad (9)$$

On the other hand, regression and correlation methods, in the context of sensitivity analysis [27], allows to indicate that \overline{W} maintains a strong relationship with St . Pearson's correlation coefficients for the log-log relationships between St and \overline{W} , Λ , ϕ and θ were -0.81, 0.19, 0.09 and -0.14, respectively. So we can roughly estimate, in first approximation,

$$\text{St} \approx \text{St}(\overline{W}). \quad (10)$$

This relative low dependence of St on Λ , ϕ and θ is due to the fact that, in most of the cases reported in Table 2, Λ is rather large while ϕ and θ vary within a relative narrow range.

Figure 5 plots the experimental results in a plane $\text{St} - \overline{W}$, not only for the present rotating wings, but also for some rotating seeds for which enough experimental data are available in the literature, clearly showing that the experimental results are approximately scaled as:

$$\overline{W} \sim \text{St}^{-1}, \quad (11)$$

with data exhibiting a certain dispersion due to the neglected dependence on Λ , ϕ , and θ . For the sake of accuracy, the exact fitting (superimposed in Figure 5) results to be $\overline{W} = 0.078807\text{St}^{-0.91455}$, with a linear regression coefficient $R^2 = 0.527$, considering seeds data for statistics in order to have a general trend.

To identify simple relationships among the dimensionless parameters in eq. (9), we use a recent scaling law by [12] that predicts that the aerodynamic force F perpendicular to the wing surface behaves as:

$$F \sim \rho \Gamma S n, \quad (12)$$

where the circulation Γ is scaled, for large aspect ratio, as [28]

$$\Gamma \sim \frac{\bar{c}V\sin(\alpha)\Lambda}{\Lambda+2}, \quad (13)$$

α being the effective angle of attack,

$$\sin(\alpha) = \frac{U}{V}, \quad V = \sqrt{U_t^2 + U^2}. \quad (14)$$

This scaling law for F was derived in the context of hovering insects with a stable LEV (i.e., when reached a stable descent velocity), so that (see background section of [12]), it seems more appropriate than a potential theory-based scaling for the present rotating wings and seeds where the LEV accounts for the high lift coefficients. Since $F\cos(\theta) \sim W$ (see Figure 4 a), $r = \phi e \cos(\theta)$ and $S = e\bar{c}$, wing loading scales as:

$$\frac{W}{S} \sim \frac{\rho U_t U}{\phi(\Lambda+2)}, \quad (15)$$

or in non-dimensional form,

$$\bar{W} \sim \frac{1}{St\phi(\Lambda+2)}. \quad (16)$$

This expression not only agrees with the scaling (10) for St , but accounts for the dependence of the non-dimensional wing loading with the rest of the relevant non-dimensional parameters. As can be seen in Figure 6, the experimental data fit well the scaling indicated by eq. (16), with a proportionality constant $m \sim 0.4$ and a coefficient of determination $R^2 = 0.6335$, including such outliers as the wing of the Umber Skipper, that rotates at a very low St (Figure 5). Moreover, the clustered data appearing in

the range $10^{-1} \leq [\text{St}\phi(\Lambda+2)]^{-1} \leq 1$ (Figure 6) might indicate propulsive optimization, as it had been observed in oscillating foils [24] and suggested for Strouhal number selection more generally by swimming and flying animals [23].

Finally, we consider relevant to pay attention to the autorotating wings performance in terms of efficiency. Norberg [1] defined the efficiency (η) of autorotating seeds as the quotient between the horizontal velocity (wing-tip speed U_t) and vertical velocities (descent speed U), i.e.

$$\eta = \frac{U_t}{U} = \frac{L}{D} = \tan^{-1}(\alpha) = 2\pi\text{St}. \quad (17)$$

This relationship corresponds to the lift-to-drag ratio (L/D) . Since η is proportional to St , we can observe that the loaded hummingbird wings and the hawkmoth wing are accordingly the most efficient wings in this sense, even more so than samaras (Table 2). By contrast, the crane-fly, the skipper, the hoverfly, and the cockroach have smaller η in comparison with other animal wings and even with plant seeds.

5. DISCUSSION

Autorotation is a widespread phenomena in nature pertaining to free-falling bodies [29]. Botanical samaras, in particular, maximize their descent time [1-3] by spinning around their center of mass, which behavior can increase their dispersal range if horizontal winds prevail. Stable rotating flight is achieved because seeds have an asymmetric mass distribution (i.e., ~80% of mass is concentrated at the wing base and the leading edge), which cause an aerodynamic torque leading to stable helical motions such the generated lift equals the summed centrifugal force and weight [14]. A constant and effective angle of attack allows a stable LEV to form and remain attached close to the seed's base [1] (Figure 7 demonstrates a comparable LEV attached to a hummingbird wing during autorotation). Here, we have

shown that multiple animal wings achieve stable autorotation and, compared to autorotating plant seeds, present a smaller negative slope for the linear relationship between wing loading and time of descent (Figure 1). Animal wings with higher loadings descend at lower rates than do plants seeds with similar loads; animal wing loadings in natural free flight are, in any event, approximately an order of magnitude larger than those of plant seeds. For example, Anna's Hummingbirds with a wing loading of $\sim 30 \text{ N/m}^2$ can flap their wings at $\sim 43 \text{ Hz}$ to generate an induced velocity of $\sim 2 \text{ m/s}$ [13], whereas a maple seed with a wing loading of $\sim 2 \text{ N/m}^2$ rotates at 18 Hz to descend at a speed of 1 m/s [3]. In spite of the major anatomical and material property differences between animal wings and samaras [for morphology details of samaras see 1, 3, 7, 14–17], both groups can perform stable autorotation at descent rates ranging from ~ 0.5 to $\sim 2 \text{ m/s}$.

One interesting result here was that a hummingbird wing loaded at the base with the equivalent of half a body mass rotated at a frequency similar to that of the free flapping frequency, and descended at the typical induced velocity (i.e., $\sim 2 \text{ m/s}$) during hovering flight [30] (see Table 1). Wings may be mechanically tuned to function at fixed oscillation rates in either spinning or flapping, if for the latter case we consider a flapping wing to be a counter-autorotating airfoil that changes spin direction between half-strokes. Pennycuik [31] suggested that bird wings work efficiently to maintain “natural” oscillation rates dependent on body mass, wing length and area, wing moment of inertia and air density. Accordingly, if all of those parameters are maintained constant between different experimental conditions, we should expect no change in flapping frequency for a given bird. Whereas muscles provide power for flapping motions, potential energy is transformed into kinetic energy during the falling of autorotating wings. The weight-specific induced power required to produce lift can be estimated from the induced velocity (in agreement with actuator disk theory; see [32]). Thus, our results on loaded hummingbirds wings indicate that autorotation can be an effective method for evaluating wing aerodynamics, because spinning wings exhibit rotational frequencies and power

dissipation similar to those in flapping flight, even though there is no stroke reversal.

Our observations of stable autorotation by dead insects, depending on wing posture, are also intriguing. Overall, lift production during autorotation in these cases should be not efficient because, while spinning, one wing presents the leading edge whereas the other wing leads with the trailing edge. However, the insect body is large relative to the wings, and associated upwards drag likely contributes to weight support. The wings also typically form a dihedral (see Video S4), contributing to stability in roll [32]. Further comparative insight are required to fully understand this phenomenon.

Major flight feathers in birds (i.e., both the primaries and secondaries) have been traditionally associated with lift production, although the secondaries may be less important. For example, sparrows without secondaries and retaining only six primaries and with an intact propatagium can flight a similar distance than sparrows with intact remiges [33]. Our experiments on hummingbird wings with secondary feathers removed showed autorotation performance equivalent to those of complete wings, consistent with the observation that the rotational axis is located at $\sim 0.2R$ where the secondaries are clustered; mass contributions of the secondaries are also very low (Figure SB, Table 1). Studies of the effects of molting on flight performance of Ruby-throated Hummingbirds have similarly shown that the secondaries are essentially irrelevant to force production [34]. However, removal of all secondaries and the first five primaries (i.e., FW-S-5P) reduced autorotating descent speed by 25% and substantially increased spinning frequency (Table 1), thus improving autorotation performance. We suggest that such aerodynamic improvement was consequence of a reduction in the moment of inertia (which can increase frequency), an increase in aspect ratio, and relocation of the center of mass more closer to the leading edge. Finally, wings with only the outer primary present (i.e., p10) were degraded in performance (Table 1), perhaps because the small ensuing wing chord impedes formation of a stable LEV. Ablation experiments on maple seeds indicate that , by contrast with hummingbird wings, descent speed is actually reduced as area removal proceeds [14]. More generally, the study of

autorotation is useful for manipulative experiments on isolated wings that otherwise are difficult to perform on alive animals, including comparative studies of the effects of feather molting, wear, and asymmetrical ablation on aerodynamic performance [35].

Dimensional analysis is an important tool to construct simple scaling laws in fluid dynamics, and specifically here for animal flight aerodynamics. Recently, Lee et al. [12] derived a scaling law for hovering insects based in the strength and momentum of vortical structures produced on the wing for lift generation. Because the LEV is an essential unsteady mechanism for lift production in autorotation [7], we followed a similar reasoning and constructed here a corresponding scaling for animal wings during autorotation. We found that inclusion of the Strouhal number, aspect ratio, and offset of the rotational axis relative to the wing base fits the previously derived law (see Lee et al. [12]; Figure 6). This similarity in the scaling of lift production in hovering flight and during wing autorotation for small animal fliers deserves further experimental attention, and particularly characterization of the LEV using Particle Image Velocimetry (PIV) or Computational Fluid Dynamics (CFD).

Finally, we conclude that isolated wings from insects and hummingbirds can autorotate during free fall as do samaras, producing substantial lift and reducing descent speed. The descent velocity U of autorotating wings (or seeds) is proportional to their wing loading W/S , inversely proportional to the tangential wing tip speed U_t (i.e., the spinning frequency times the radius of gyration), and directly proportional to the offset of the rotational axis relative to the base of the wing (parameter ϕ). On the other hand, the relevance of the wing aspect ratio is also noteworthy Λ , given the diversity of wing shapes analyzed in this work. Both ϕ and Λ are required to obtain a strong statistical fit to the experimental data.

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AUTHOR CONTRIBUTIONS

Conceived the idea: VMO-J. Designed the experiments: VMO-J, RD. Performed the experiments: VMO-J, AM-A. Analyzed the data: VMO-J, AM-A, RF-F. Theoretical analysis: RF-F, AM-A. Wrote the paper: VMO-J, RD, AM-A, RF-F.

COMPETING INTERESTS

We declare no competing interests.

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FIGURES

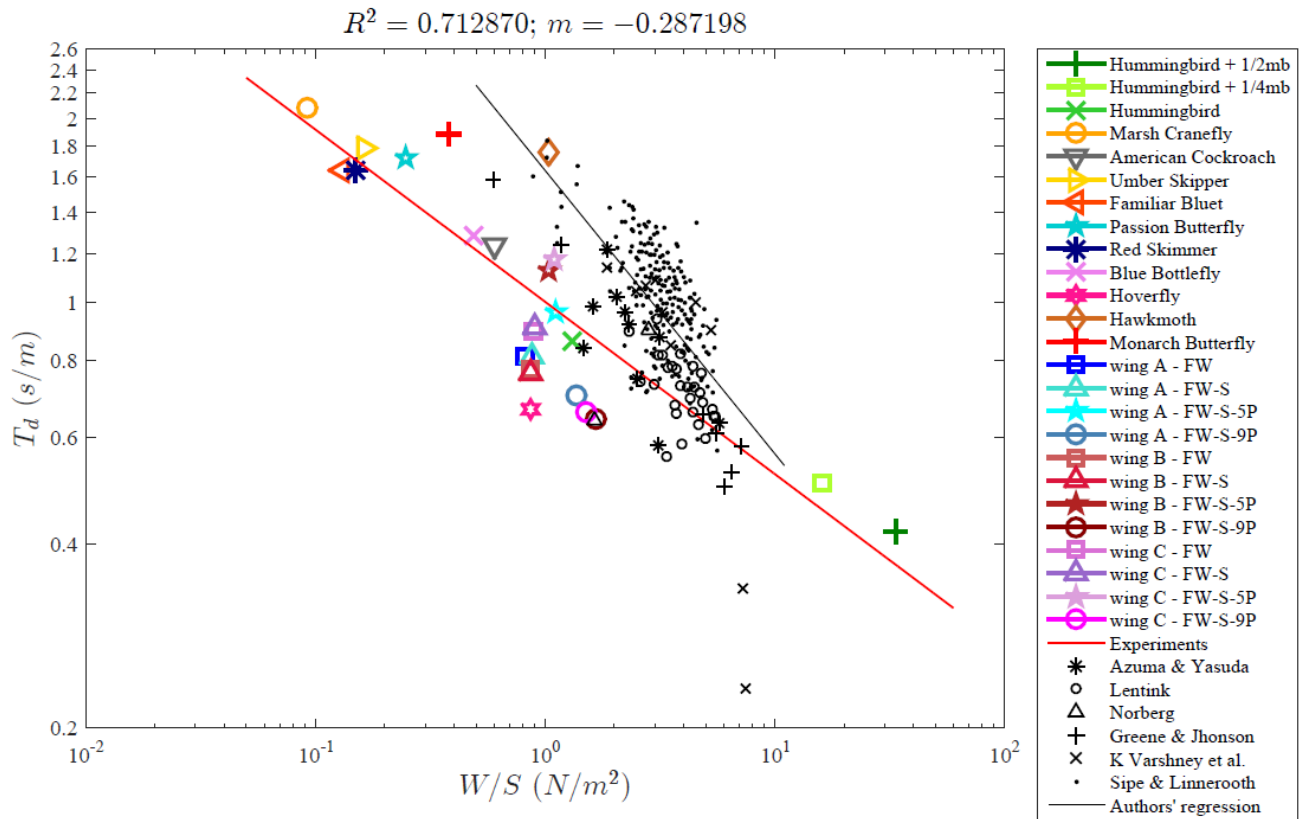


Figure 1. Log-log plot of wing loading versus descent time per meter of animal wings (in color) and plant seeds (in black) during autorotation. Linear fits of data for animal wings and plant seeds are represented by a red line ($\log Y = -0.28 \log(X) - 0.02$, $r^2 = 0.71$, $F_{1,23} = 57.1$, $p < 0.001$) and by a black line ($\log Y = -0.46 \log X + 0.22$, $r^2 = 0.42$, $F_{1,264} = 190.3$, $p < 0.001$), respectively. Data on seeds were obtained from published literature [1, 3, 7, 12-15]. Data on animal wings includes those generated during wing feather removal (blue circle) and supplemental loading experiments. See text for details.

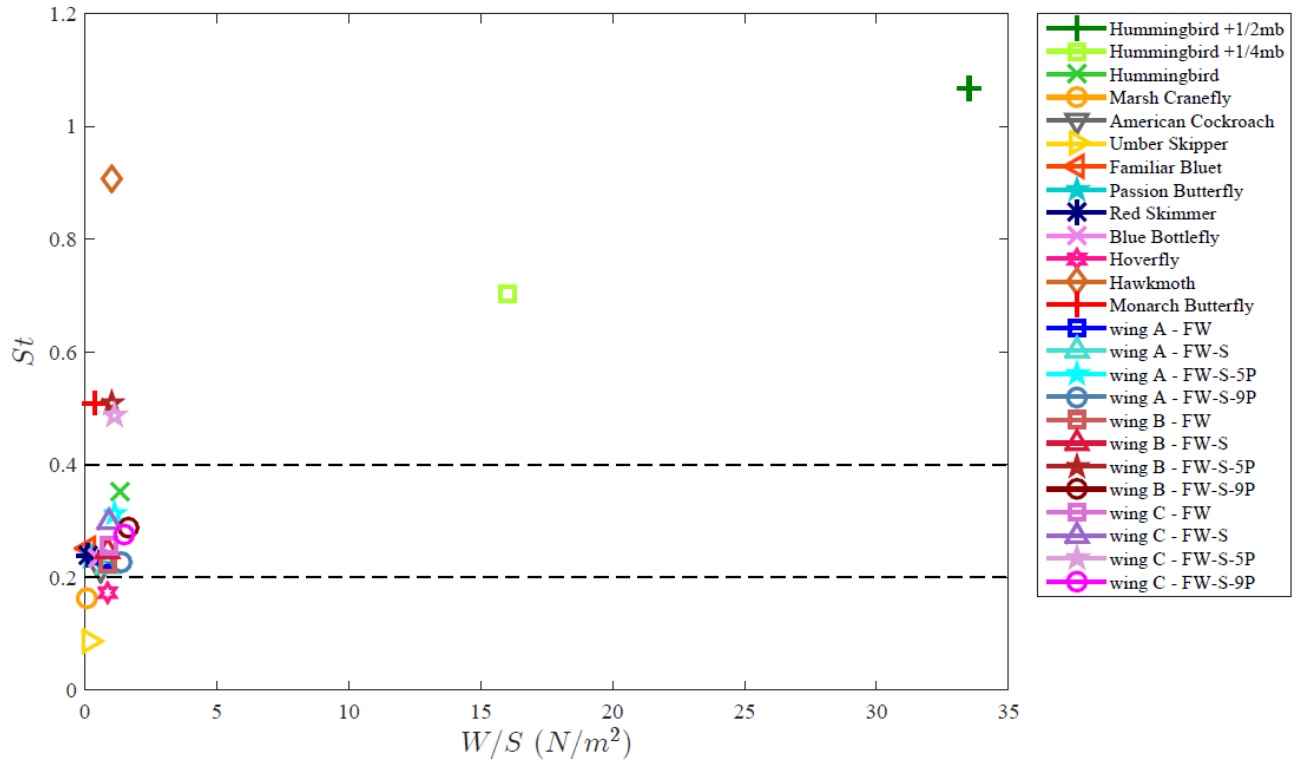


Figure 2: Autorotation performance of Anna's hummingbird wings ($N=3$) with sequential feather removal, including descent speed (A), rotational frequency (B), coning angle (C), and wing tip speed (D): complete wing FW, wing without secondaries -S, wing without secondaries and five inner primaries -S-5P, wing with only one primary -S-9P. Error bars indicate one standard deviation.

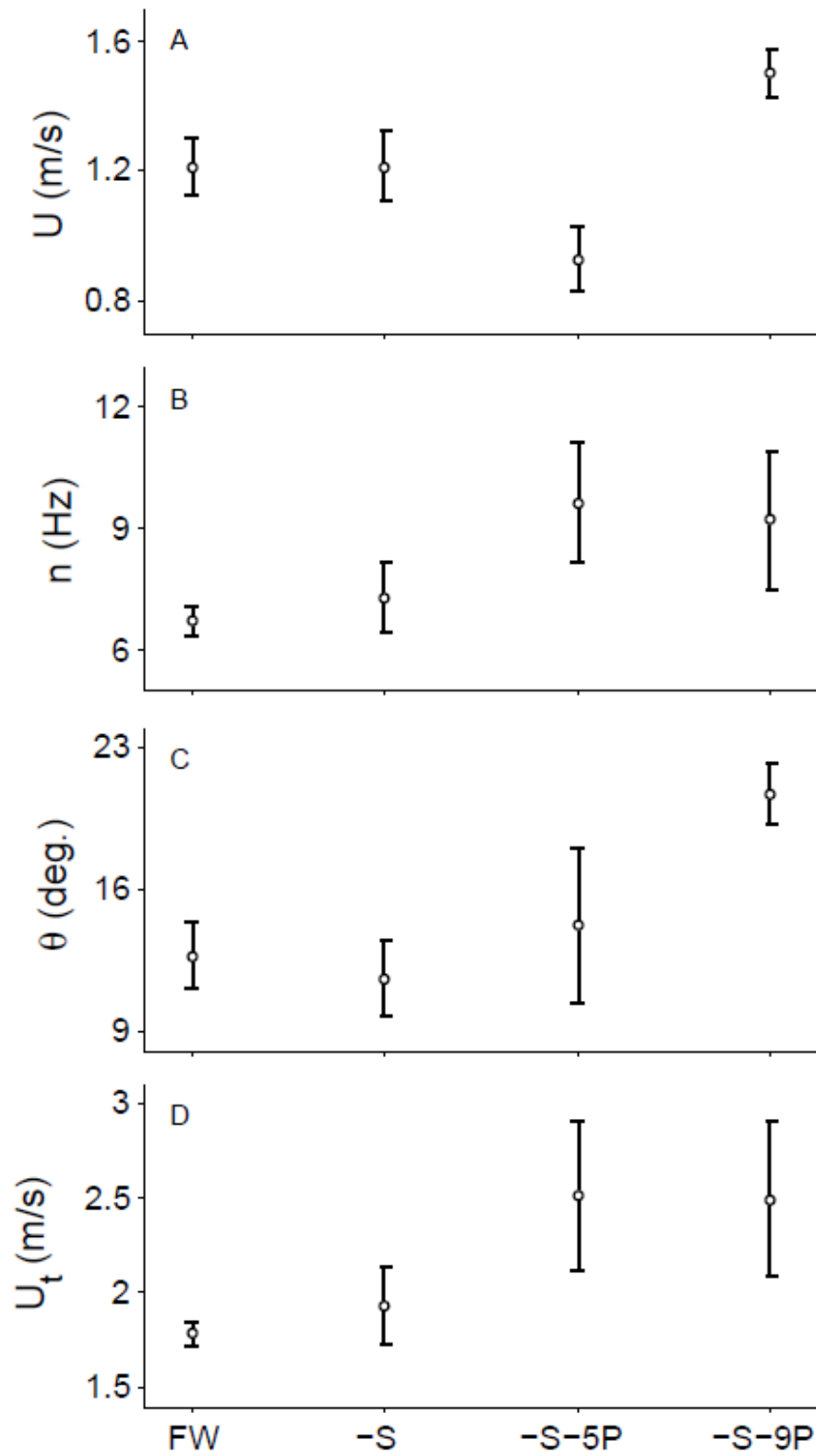


Figure 3: Dimensional wing loading W/S vs. the Strouhal number of animal wings during autorotation. The dashed black lines indicate the range $0.2 \leq St \leq 0.4$.

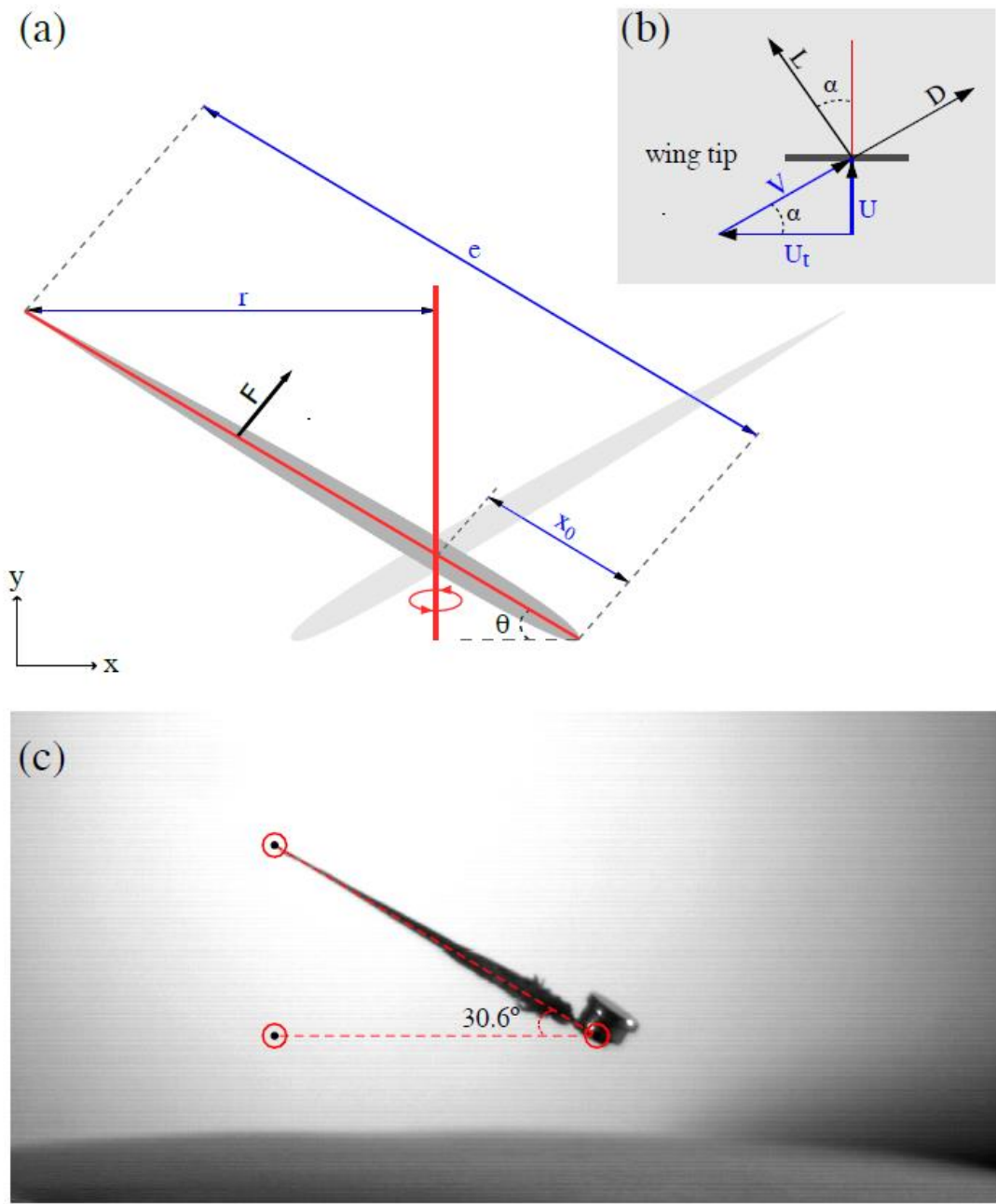


Figure 4: (a) Sketch of the lateral view of an autorotating wing; (b) frontal sketch of the wing tip showing relative velocities; (c) Example of assessment of the coning angle of a loaded Anna's hummingbird wing in autorotating motion.

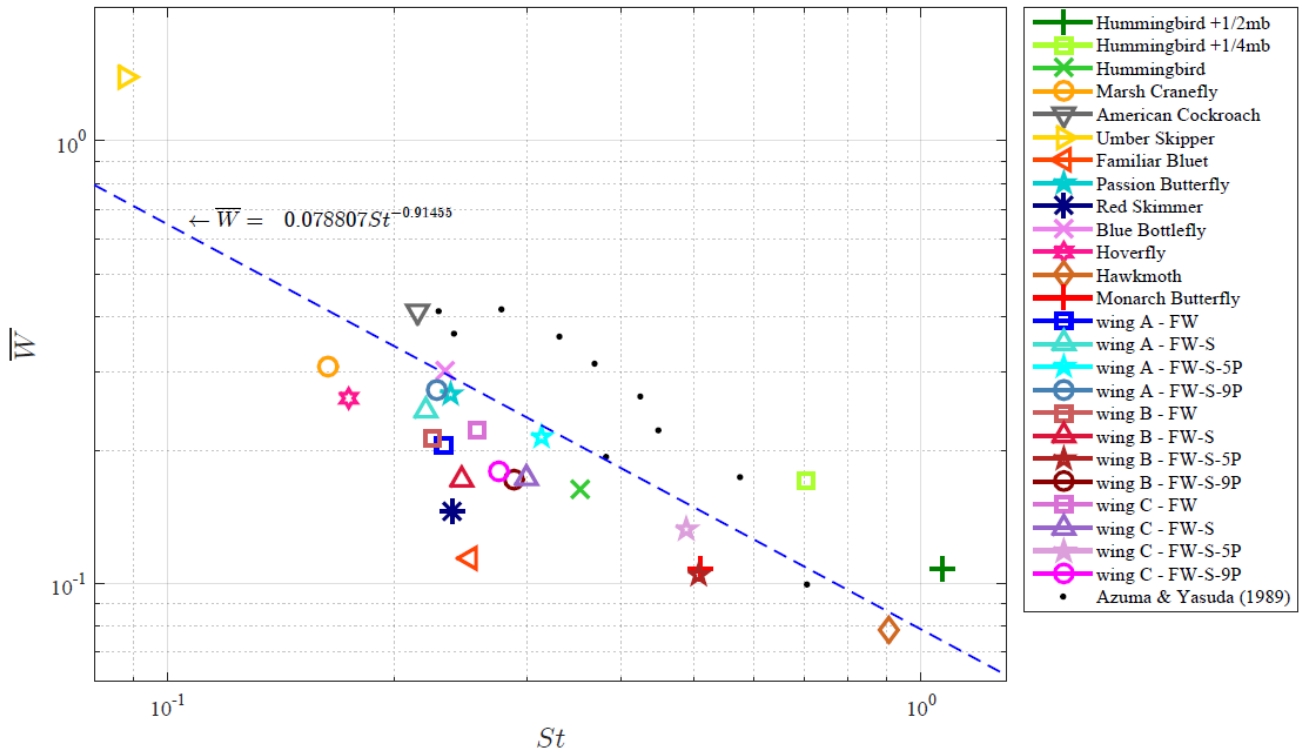


Figure 5: Logarithmic plot of the non-dimensional wing loading \bar{W} vs. St , with the blue dashed line indicating the curve $\bar{W} = 0.078807St^{-0.91455}$ ($R^2 = 0.527$ $F_{1,33} = 39$, $p < 0.001$). Among all seed data plotted in Fig. 1, only those in ref. [3] provide sufficient data for inclusion here.

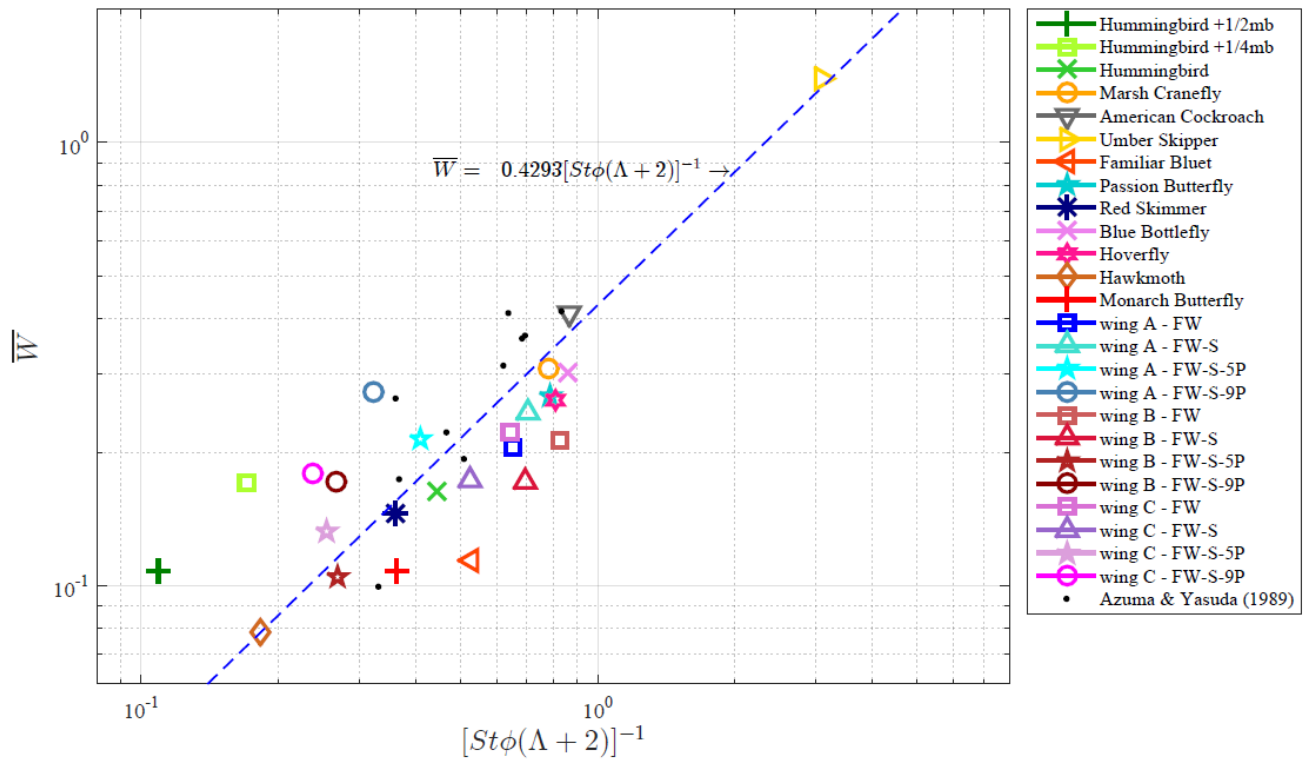


Figure 6: Logarithmic plot of dimensionless wing loading vs. the scaling parameter obtained in eq. (16). Among all seed data plotted in Fig. 1, only those in ref. [3] provide sufficient data for inclusion here. Blue-dashed line indicates regression ($R^2 = 0.6335$ $F_{1,33} = 57$, $p < 0.001$).

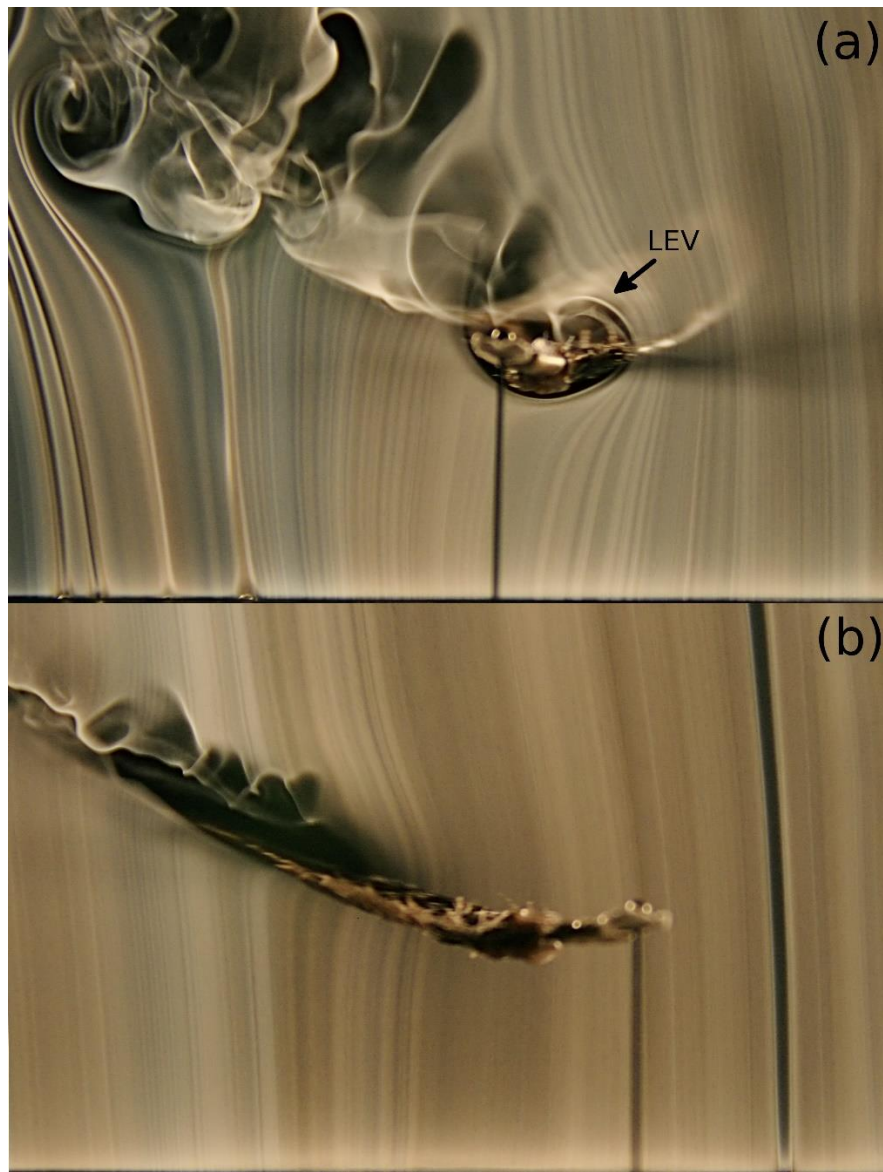


Figure 7: Smoke visualization of a male Anna's Hummingbird wing in autorotation. A wire was placed in the rotation-axis to force a fixed position in the vertical wind tunnel. A compact leading edge vortex LEV is clearly visible close to the wing base (A), but not near the wing tip (B).

SUPPLEMENTARY MATERIAL



Figure SA. Sampled insect wings, from top left to right bottom: Monarch Butterfly, Passion Butterfly, Hawkmoth, Red Skimmer, American Cockroach, Umber Skipper, Marsh Cranefly, Familiar Bluet, Bluebottle Fly and Syrphus Hoverfly.



Figure SB. Anna's Hummingbird wing following sequential feather removal: full wing, FW; wing without secondaries, FW-S; wing without secondaries and without five inner primaries, FW-S-5P; wing with only one primary, FW-S-9P.



Figure SC. Anna's hummingbird wing with extra load of one-half body mass fixed at the wing base.

VIDEOS

[VideoS1.mp4](#) [Autorotation performance of wings from ten insect taxa]

[VideoS2.mp4](#) [Autorotation performance of an Anna's hummingbird wing after feather removal]

[VideoS3.mp4](#) [Autorotation performance of an unloaded Anna's hummingbird wing, and then loaded with a quarter of and then one-half of body mass]

[VideoS4.mp4](#) [Whole-body autorotation of a hawkmoth and hoverfly]