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**Fracture and Damage Mechanics**

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**Seville, Spain**

## **Numerical analysis of the pivot node in fracture problems**

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# Numerical analysis of the pivot node in fracture problems

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Line of research: Develop a finite element methodology to improve the accuracy in the evaluation of 3-D phenomenon near the crack in fatigue simulation.



Fatigue simulation focused on crack closure determination.



Fracture simulation focused on stress intensity factor determination



Crack closure criteria

Mesh density

SIF calculation criteria

INVOLVED FACTORS  
Cross-influence?

Contact simulation

Plastic wake generation

Crack shape

FEM simulations (Ansys software) with:

- CT specimen.
- Mode I load
- Aluminum 2024-T35 material
- No previous plastic wake generated

Objectives:

- Mesh requirement
- COD vs J-integral  $K_I$  determination
- Thickness, load level and crack shape influence
- 3-D effects through thickness
- Influence on fatigue parameters

Pivot node ( $P_1$ ) identification



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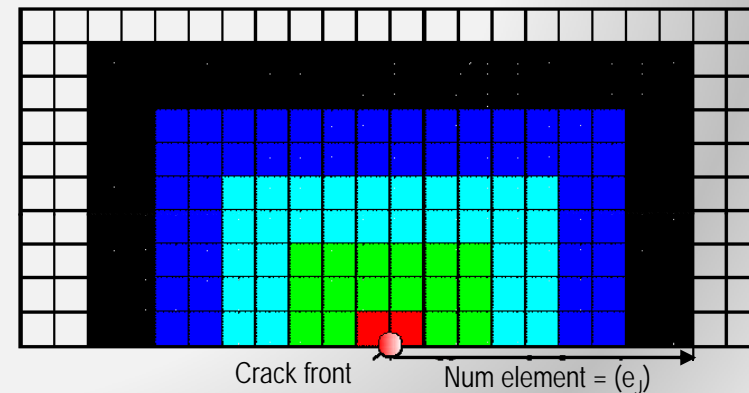
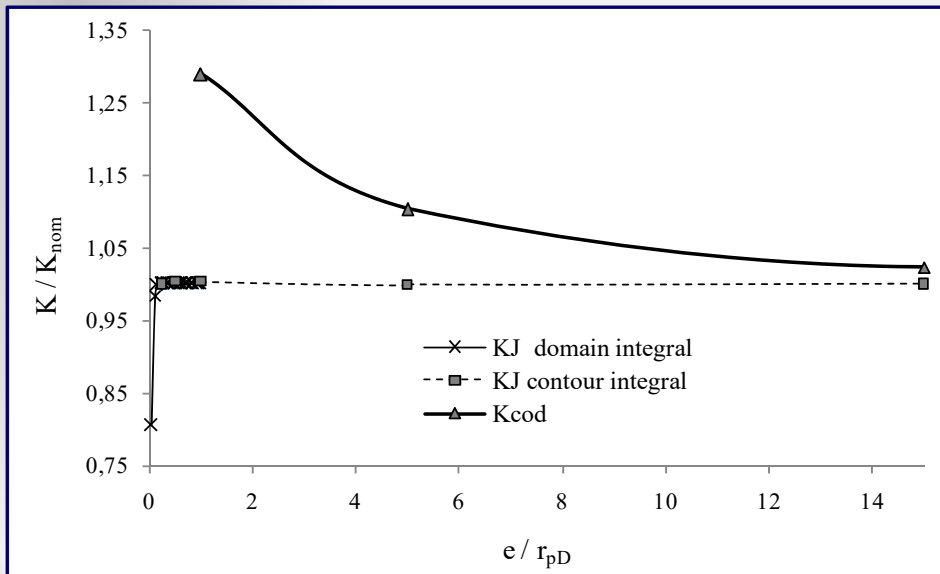
## K<sub>I</sub> calculation <sup>(1)(2)</sup>

3-D evolution related to the nominal one ( $K_{nom}$ )  
 J-integral presents better accuracy that COD methods to detect tridimensional variations near the crack ( $K_J$ )  
 Plane strain hypothesis ( $b=3-12mm$ ,  $K_{nom}=10-40MPa\ m^{1/2}$ )

$$K_{nom} = \frac{P}{B\sqrt{W}} \left\{ \frac{2 + \frac{a}{W}}{\left(1 - \frac{a}{W}\right)^{\frac{3}{2}}} \left[ 0.886 + 4.64 \cdot \left(\frac{a}{W}\right) - 13.32 \cdot \left(\frac{a}{W}\right)^2 \right] + 14.72 \cdot \left(\frac{a}{W}\right)^3 - 5.6 \cdot \left(\frac{a}{W}\right)^4 \right\}$$

$$J = \int_A \left( \sigma_{ij} \frac{\partial u_j}{\partial x_i} + w \delta_{ii} \right) \frac{\partial q}{\partial x_i} dA$$

$$K_J = \sqrt{J \frac{E}{(1+\nu^2)}}$$



- Garcia-Manrique, J., Camas, D., Lopez-Crespo, P., Gonzalez-Herrera, A. Stress intensity factor analysis of through thickness effects. Int J Fatigue 2013; 46:58-66.
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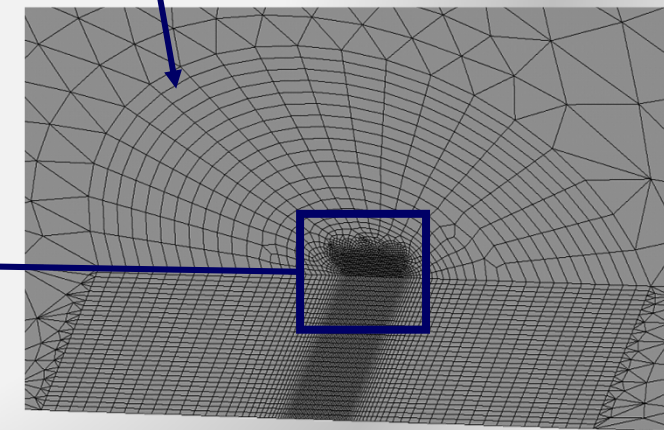
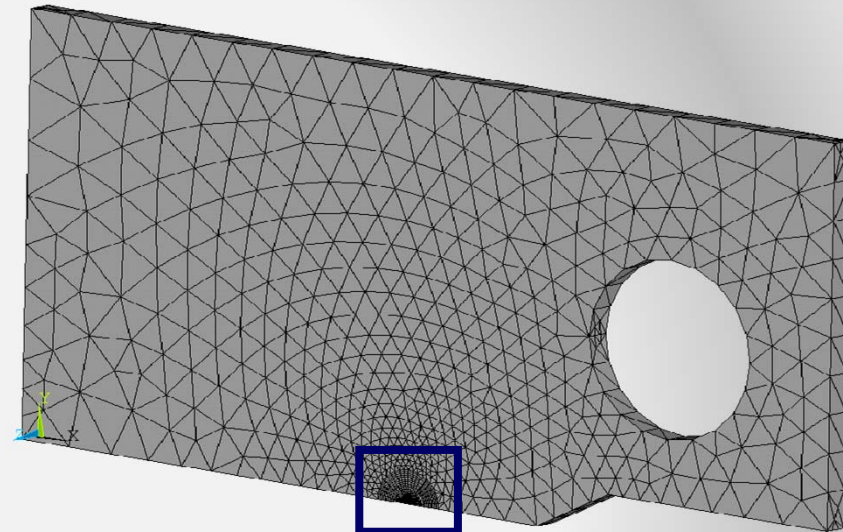
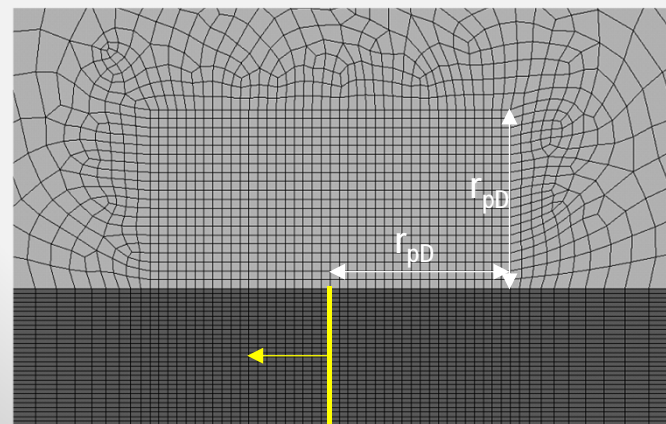
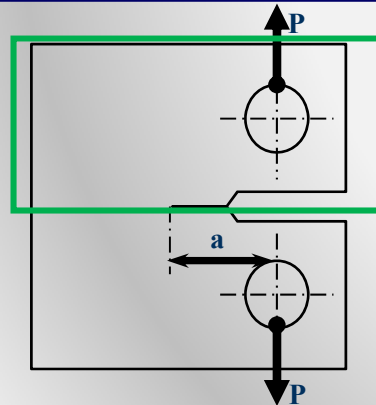
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## Mesh conditions<sup>(1)(2)</sup>

Mesh density proportional to the applied load.

Regular meshing around the crack. Progressive to surface

Linear element selection (SOLID185 in ansys code)



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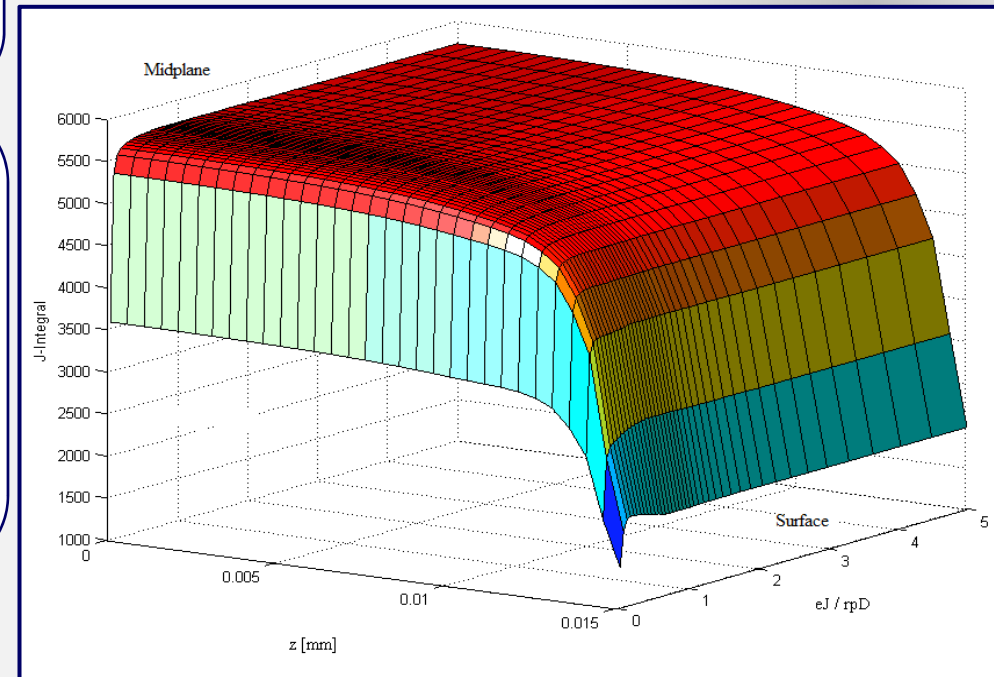
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Analysis of minimum element size near the crack. Both in crack direction ( $t_{mex} < 1/20 r_{pD}$ ) and through thickness ( $t_{mez} < 1/40 b$ ).



Influence of distance  $e_j$  in the J-integral calculation through thickness in 3D simulation.  
( $K_{nom} = 20 \text{ MPa} \cdot \text{m}^{1/2}$ ,  $b=3\text{mm}$ ,  $a=20\text{mm}$ )

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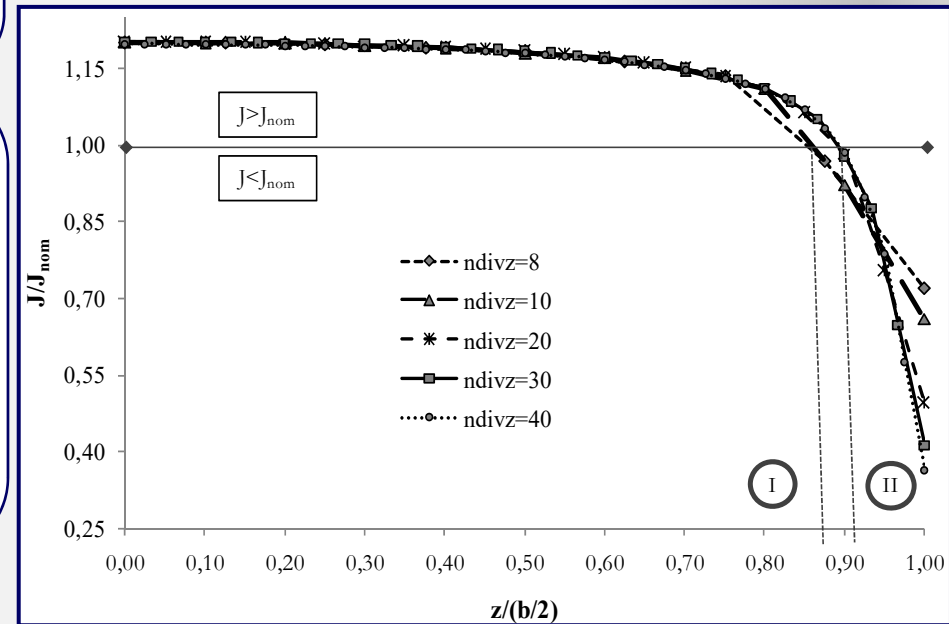
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Evolution of J-integral through thickness in a straight crack front for different mesh densities ( $K_{nom} = 20 \text{MPa} \cdot \text{m}^{1/2}$ ,  $b=3\text{mm}$ ,  $a=20\text{mm}$ )

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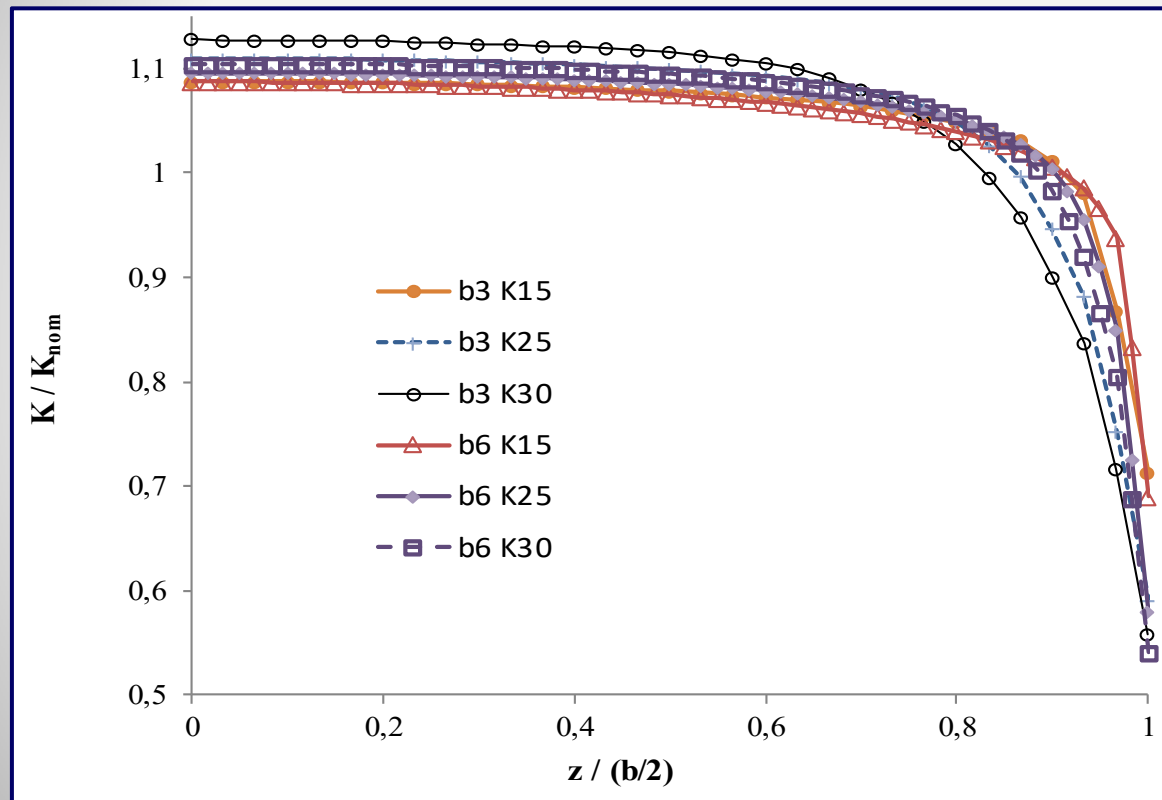
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## Pivot node <sup>(3)</sup>

Some results to study the influence of thickness and maximum load in  $K_j$  distribution. Non-dimensionalized with  $K_{nom}$  and thickness  $(b/2)$ .



Stress intensity factor distribution in straight crack front. Thickness  $b= 3$  mm and  $b= 6$  mm.  $K_{max}=15, 25$  and  $30$  MPam<sup>1/2</sup>. Non-dimensionalized results along the thickness.

3. J. Garcia-Manrique, D. Camas-Peña, J. Lopez-Martinez, A. Gonzalez-Herrera, Analysis of the stress intensity factor along the thickness: The concept of pivot node on straight crack fronts, Fatigue Fract. Eng. Mater. Struct. 41 (2018).



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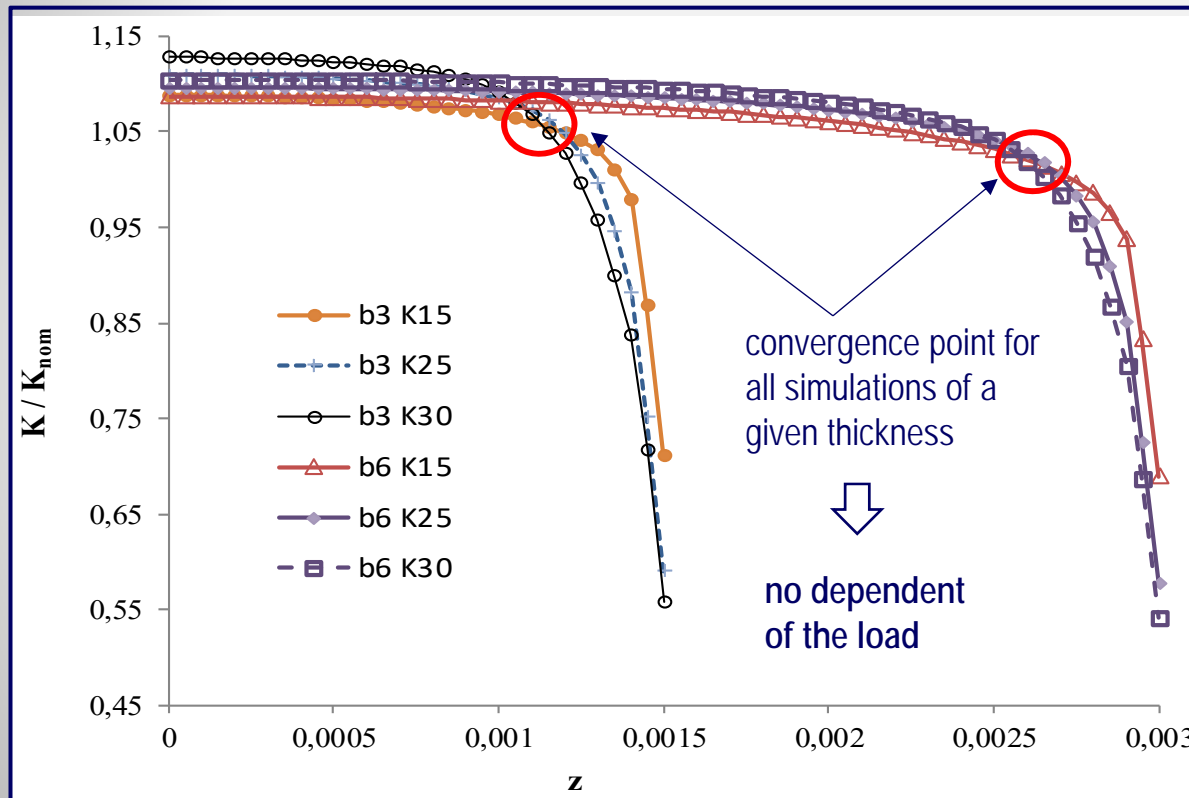
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Some results to study the influence of thickness and maximum load in  $K_j$  distribution. *Non-dimensionalized with  $K_{nom}$*



sustained growth?  
crack front shape would pivot around it?

Stress intensity factor distribution in straight crack front. Thickness  $b= 3$  mm and  $b= 6$  mm.  $K_{max}=15, 25$  and  $30$  MPam<sup>1/2</sup>. Results along the thickness.

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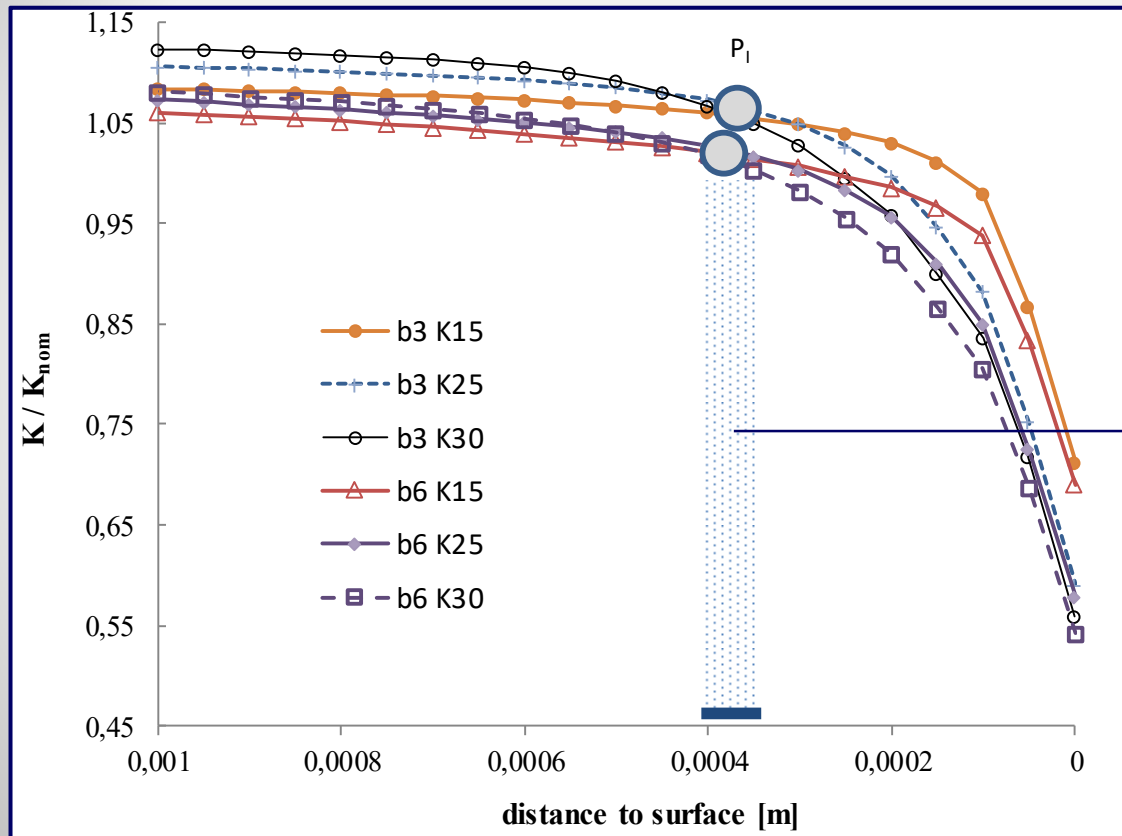
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## Pivot node <sup>(3)</sup>

Some results to study the influence of thickness and maximum load in  $K_j$  distribution. X-axis : distance to surface



located at the same distance from the exterior  
↓  
no dependent of the total thickness

Opportunity to improve the correlation of numerical and experimental results

Stress intensity factor distribution in straight crack front versus distance to the surface. Thickness  $b= 3$  mm and  $b= 6$  mm.  $K_{max}=15, 25$  and  $30$  MPam<sup>1/2</sup>.

3. J. Garcia-Manrique, D. Camas-Peña, J. Lopez-Martinez, A. Gonzalez-Herrera, Analysis of the stress intensity factor along the thickness: The concept of pivot node on straight crack fronts, Fatigue Fract. Eng. Mater. Struct. 41 (2018).



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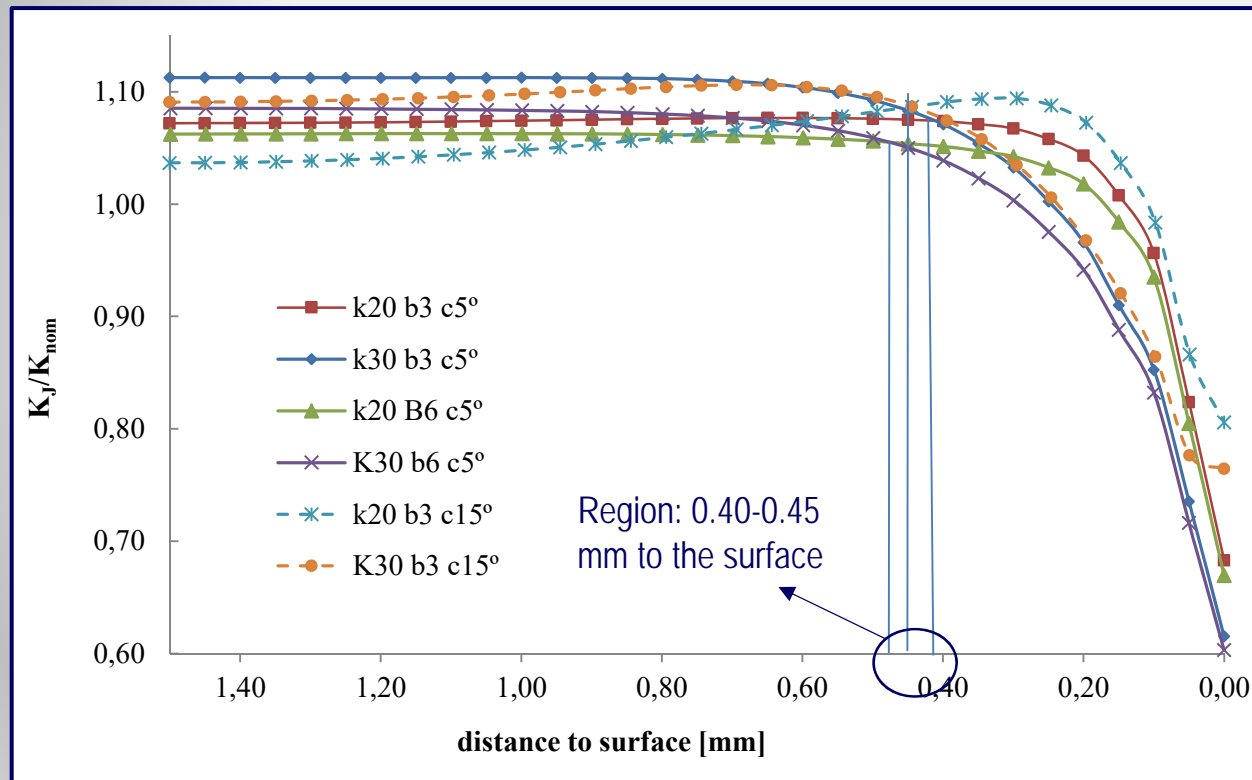
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## Pivot node

Some results to study the influence of crack shape curvature in the location of pivot node



Stress intensity factor distribution in curve crack front versus distance to the surface. Thickness  $b = 3$  mm and  $b = 6$  mm. Curvature  $5^\circ$  and  $15^\circ$ .  $K_{\max} = 20$  and  $30 \text{ MPam}^{1/2}$ .



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## CONCLUSION

Through FEM evaluation of  $K_I$ , we can identify a narrow region where the binomial influence of load level and thickness disappear.

It becomes a region that characterizes the crack growth phenomenon and presents interesting characteristics for the numerical-experimental correlation.

THANK YOU FOR YOUR ATTENTION